

European Technical Approval ETA-98/0001

English translation prepared by DIBt - Original version in German language Handelsbezeichnung Hilti Durchsteckanker HST, HST-R und HST-HCR Trade name Hilti stud anchor HST, HST-R and HST-HCR Zulassungsinhaber Hilti Aktiengesellschaft **Business Unit Anchors** Holder of approval 9494 Schaan FÜRSTENTUM LIECHTENSTEIN Zulassungsgegenstand Kraftkontrolliert spreizender Dübel in den Größen M8, M10, und Verwendungszweck M12, M16, M20 und M24 zur Verankerung im Beton Generic type and use Torque controlled expansion anchor of sizes M8, M10, M12, M16, M20 and M24 for use in concrete of construction product Geltungsdauer: 18 November 2008 vom Validity: from bis 19 February 2013 to Herstellwerk Hilti Aktiengesellschaft Manufacturing plant Werk 1

Diese Zulassung umfasst This Approval contains

Diese Zulassung ersetzt This Approval replaces



ETA-98/0001 with validity from 12.02.2008 to 19.02.2013

ETA-98/0001 mit Geltungsdauer vom 12.02.2008 bis 19.02.2013

Europäische Organisation für Technische Zulassungen European Organisation for Technical Approvals

22 Seiten einschließlich 14 Anhänge

22 pages including 14 annexes

I LEGAL BASES AND GENERAL CONDITIONS

- 1 This European technical approval is issued by Deutsches Institut für Bautechnik in accordance with:
 - Council Directive 89/106/EEC of 21 December 1988 on the approximation of laws, regulations and administrative provisions of Member States relating to construction products¹, modified by Council Directive 93/68/EEC² and Regulation (EC) N° 1882/2003 of the European Parliament and of the Council³;
 - Gesetz über das In-Verkehr-Bringen von und den freien Warenverkehr mit Bauprodukten zur Umsetzung der Richtlinie 89/106/EWG des Rates vom 21. Dezember 1988 zur Angleichung der Rechts- und Verwaltungsvorschriften der Mitgliedstaaten über Bauprodukte und anderer Rechtsakte der Europäischen Gemeinschaften (Bauproduktengesetz - BauPG) vom 28. April 1998⁴, zuletzt geändert durch Gesetz vom 06.01.2004⁵;
 - Common Procedural Rules for Requesting, Preparing and the Granting of European technical approvals set out in the Annex to Commission Decision 94/23/EC⁶;
 - Guideline for European technical approval of "Metal anchors for use in concrete Part 2: Torque controlled expansion anchors ", ETAG 001-02.
- 2 Deutsches Institut für Bautechnik is authorized to check whether the provisions of this European technical approval are met. Checking may take place in the manufacturing plant. Nevertheless, the responsibility for the conformity of the products to the European technical approval and for their fitness for the intended use remains with the holder of the European technical approval.
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¹ Official Journal of the European Communities L 40, 11.02.1989, p. 12

² Official Journal of the European Communities L 220, 30.08.1993, p. 1

³ Official Journal of the European Union L 284, 31.10.2003, p. 25

⁴ Bundesgesetzblatt I, p. 812

⁵ Bundesgesetzblatt I, p.2, 15

⁶ Official Journal of the European Communities L 17, 20.01.1994, p. 34

II SPECIFIC CONDITIONS OF THE EUROPEAN TECHNICAL APPROVAL

1 Definition of product and intended use

1.1 Definition of the construction product

The Hilti stud anchor HST, HST-R and HST-HCR is an anchor made of galvanised steel (designated as HST) or stainless steel (designated as HST-R) of sizes M8, M10, M12, M16, M20 and M24 or made of high corrosion resistant steel (designated as HST-HCR) of sizes M8, M10, M12 and M16 which is placed into a drilled hole and anchored by torque-controlled expansion.

An illustration of the product and intended use is given in Annex 1.

1.2 Intended use

The anchor is intended to be used for anchorages for which requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 of Council Directive 89/106 EEC shall be fulfilled and failure of anchorages made with these products would cause risk to human life and/or lead to considerable economic consequences.

The anchor may be used for anchorages with requirements related to resistance to fire.

The anchor is to be used only for anchorages subject to static or quasi-static loading in reinforced or unreinforced normal weight concrete of strength classes C20/25 at minimum and C50/60 at most according to EN 206:2000-12.

It may be anchored in cracked and non-cracked concrete.

Hilti Stud Anchor HST made of galvanised steel:

The anchor may only be used in structures subject to dry internal conditions.

Hilti Stud Anchor HST-R made of stainless steel A4:

The anchor made of stainless steel A4 may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure (including industrial and marine environment), or exposure in permanently damp internal conditions, if no particular aggressive conditions exist. Such particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

Hilti Stud Anchor HST-HCR made of high corrosion resistant steel:

The anchor made of high corrosion resistant steel may be used in structures subject to dry internal conditions and also in structures subject to external atmospheric exposure, in permanently damp internal conditions or in other particular aggressive conditions. Such particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

The provisions made in this European technical approval are based on an assumed working life of the anchor of 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

2 Characteristics of the product and methods of verification

2.1 Characteristics of the product

The anchor corresponds to the drawings and provisions given in Annexes 2 and 3. The characteristic material values, dimensions and tolerances of the anchor not given in Annexes 2 and 3 shall correspond to the respective values laid down in the technical documentation⁷ of this European technical approval.

Regarding the requirements concerning safety in case of fire it is assumed that the anchor meets the requirements of class A1 in relation to reaction to fire in accordance with the stipulations of the Commission decision 96/603/EC, amended by 2000/605/EC.

The characteristic values for the design of anchorages are given in Annexes 4 to 9.

The characteristic values for the design of anchorages regarding resistance to fire are given in the Annexes 10 to 14. They are valid for use in a system that is required to provide a specific fire resistance class.

Each anchor is marked with the identifying mark of the producer, the anchor identity, the size of thread and the maximum thickness of fixture according to Annex 1. In addition, the minimum anchorage depth is marked on the bolt. Each anchor made of stainless steel A4 is marked with the letter "-R" and each anchor made of high corrosion resistant steel is marked with the letters "-HCR".

The anchor shall only be packaged and supplied as a complete unit.

2.2 Methods of verification

The assessment of fitness of the anchor for the intended use in relation to the requirements for mechanical resistance and stability and safety in use in the sense of the Essential Requirements 1 and 4 has been made in accordance with the "Guideline for European technical approval of Metal Anchors for Use in Concrete", Part 1 "Anchors in general" and Part 2 "Torque-controlled expansion anchors", on the basis of Option 1.

The assessment of the anchor for the intended use in relation to the requirements for resistance to fire has been made in accordance with the Technical Report TR 020 "Evaluation of anchorages in concrete concerning resistance to fire".

In addition to the specific clauses relating to dangerous substances contained in this European technical approval, there may be other requirements applicable to the products falling within its scope (e.g. transposed European legislation and national laws, regulations and administrative provisions). In order to meet the provisions of the Construction Products Directive, these requirements need also to be complied with, when and where they apply.

7

The technical documentation of this European technical approval is deposited at the Deutsches Institut für Bautechnik and, as far as relevant for the tasks of the approved bodies involved in the attestation of conformity procedure, is handed over to the approved bodies.

3 Evaluation and attestation of conformity and CE marking

3.1 System of attestation of conformity

According to the decision 96/582/EG of the European Commission⁸ the system 2(i) (referred to as system 1) of attestation of conformity applies.

System 1: Certification of the conformity of the product by an approved certification body on the basis of:

- (a) Tasks for the manufacturer:
 - (1) factory production control;
 - (2) further testing of samples taken at the factory by the manufacturer in accordance with a prescribed test plan;
- (b) Tasks for the approved body:
 - (3) initial type-testing of the product;
 - (4) initial inspection of factory and of factory production control;
 - (5) continuous surveillance, assessment and approval of factory production control.

Note: Approved bodies are also referred to as "notified bodies".

3.2 **Responsibilities**

- 3.2.1 Tasks of the manufacturer
- 3.2.1.1 Factory production control

The manufacturer shall exercise permanent internal control of production. All the elements, requirements and provisions adopted by the manufacturer shall be documented in a systematic manner in the form of written policies and procedures, including records of results performed. This production control system shall insure that the product is in conformity with this European technical approval.

The manufacturer may only use initial/ raw/ constituent materials stated in the technical documentation of this European technical approval.

The factory production control shall be in accordance with the control plan of February 2008 which is part of the technical documentation of this European technical approval. The control plan is laid down in the context of the factory production control system operated by the manufacturer and deposited at Deutsches Institut für Bautechnik⁹.

The results of factory production control shall be recorded and evaluated in accordance with the provisions of the control plan.

3.2.1.2 Other tasks of manufacturer

The manufacturer shall, on the basis of a contract, involve a body which is approved for the tasks referred to in section 3.1 in the field of anchors in order to undertake the actions laid down in section 3.2.2. For this purpose, the control plan referred to in sections 3.2.1.1 and 3.2.2 shall be handed over by the manufacturer to the approved body involved.

The manufacturer shall make a declaration of conformity, stating that the construction product is in conformity with the provisions of this European technical approval.

⁸ Official Journal of the European Communities L 254 of 08.10.1996.

⁹ The control plan is a confidential part of the documentation of the European technical approval, but not published together with the ETA and only handed over to the approved body involved in the procedure of attestation of conformity. See section 3.2.2.

3.2.2 Tasks of approved bodies

The approved body shall perform the

- initial type-testing of the product,
- initial inspection of factory and of factory production control,
- continuous surveillance, assessment and approval of factory production control,

in accordance with the provisions laid down in the control plan.

The approved body shall retain the essential points of its actions referred to above and state the results obtained and conclusions drawn in a written report.

The approved certification body involved by the manufacturer shall issue an EC certificate of conformity of the product stating the conformity with the provisions of this European technical approval.

In cases where the provisions of the European technical approval and its control plan are no longer fulfilled the certification body shall withdraw the certificate of conformity and inform Deutsches Institut für Bautechnik without delay.

3.3 CE marking

The CE marking shall be affixed on each packaging of the anchor. The letters "CE" shall be followed by the identification number of the approved certification body, where relevant, and be accompanied by the following additional information:

- the name and address of the producer (legal entity responsible for the manufacturer),
- the last two digits of the year in which the CE marking was affixed,
- the number of the EC certificate of conformity for the product,
- the number of the European technical approval,
- the number of the guideline for European technical approval
- use category (ETAG 001-1 Option 1),
- size.

4 Assumptions under which the fitness of the product for the intended use was favourably assessed

4.1 Manufacturing

The European technical approval is issued for the product on the basis of agreed data/information, deposited with the Deutsches Institut für Bautechnik, which identifies the product that has been assessed and judged. Changes to the product or production process, which could result in this deposited data/information being incorrect, should be notified to the Deutsches Institut für Bautechnik before the changes are introduced. Deutsches Institut für Bautechnik will decide whether or not such changes affect the approval and consequently the validity of the CE marking on the basis of the approval and if so whether further assessment or alterations to the approval shall be necessary.

4.2 Installation

4.2.1 Design of anchorages

The fitness of the anchor for the intended use is given under the following conditions:

The anchorages are designed in accordance with the "Guideline for European technical approval of Metal Anchors for Use in Concrete", Annex C, Method A, under the responsibility of an engineer experienced in anchorages and concrete work.

Verifiable calculation notes and drawings are taking account of the loads to be anchored.

The position of the anchor is indicated on the design drawings (e.g. position of the anchor relative to reinforcement or to supports).

The design of anchorages under fire exposure has to consider the conditions given in the Technical Report TR 020 "Evaluation of anchorages in concrete concerning resistance to fire". The relevant characteristic anchor values are given in Annexes 10 to 14. The design method covers anchors with a fire attack from one side only. If the fire attack is from more than one side, the design method may be taken only, if the edge distance of the anchor is $c \ge 300$ mm.

4.2.2 Installation of anchors

The fitness for use of the anchor can only be assumed if the anchor is installed as follows:

- Anchor installation carried out by appropriately qualified personnel and under the supervision of the person responsible for technical matters of the site,
- Use of the anchor only as supplied by the manufacturer without exchanging the components of an anchor,
- Anchor installation in accordance with the manufacturer's specifications and drawings and using the appropriate tools,
- Checks before placing the anchor to ensure that the strength class of the concrete in which the anchor is to be placed is in the range given and is not lower than that of the concrete to which the characteristic loads apply,
- Check of concrete being well compacted, e.g. without significant voids,
- Edge distances and spacings not less than the specified values without minus tolerances,
- Positioning of the drill holes without damaging the reinforcement,
- In case of aborted hole: new drilling at a minimum distance away of twice the depth of the aborted hole or smaller distance if the aborted drill hole is filled with high strength mortar and if under shear or oblique tension load it is not in the direction of load application,
- Cleaning of the hole of drilling dust,
- Anchor installation such that the effective anchorage depth is complied with. This compliance is ensured when the embedment mark of the anchor does no more exceed the concrete surface,
- Application of the torque moment given in Annex 3 using a calibrated torque wrench.

4.2.3 Responsibility of the manufacturer

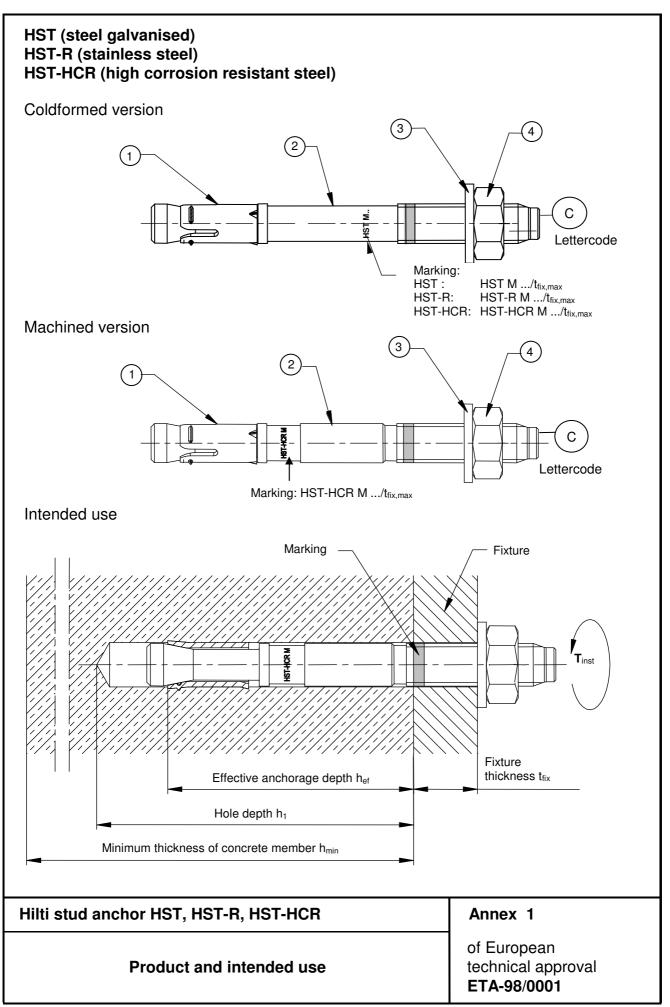
The manufacturer is responsible to ensure that the information on the specific conditions according to 1 and 2 including Annexes referred to and 4.2.1 and 4.2.2 is given to those who are concerned. This information may be made by reproduction of the respective parts of the European technical approval. In addition all installation data shall be shown clearly on the package and/or on an enclosed instruction sheet, preferably using illustration(s).

The minimum data required are:

- Diameter of drill bit,
- Thread diameter,
- Maximum thickness of the fixture,
- Minimum effective anchorage depth,
- Minimum hole depth,
- Torque moment,
- Information on the installation procedure, including cleaning of the hole, preferably by means of an illustration,
- Reference to any special installation equipment needed,
- Identification of the manufacturing batch.

All data shall be presented in a clear and explicit form.

Dipl.-Ing. E. Jasch President of Deutsches Institut für Bautechnik Berlin, 18 November 2008 *beglaubigt:* Lange



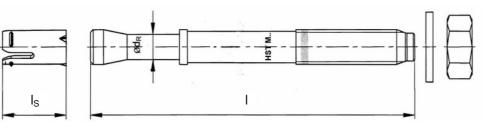
Part	Designation	Mate	erial
IST	(steel galvanised)		
1	Expansion sleeve	Stainless steel A4	
		Carbon steel galvanised and coated	
2	Bolt	M16 $f_{uk} = 72$ M20: $f_{uk} = 70$	$\begin{array}{l} \text{D0N/mm}^2, \ f_{yk} = 640\text{N/mm}^2\\ \text{20N/mm}^2, \ f_{yk} = 580\text{N/mm}^2\\ \text{D0N/mm}^2, \ f_{yk} = 560\text{N/mm}^2\\ \text{30N/mm}^2, \ f_{yk} = 450\text{N/mm}^2 \end{array}$
3	Washer	Steel galvanised, EN ISO 4042	
4	Hexagon nut	Class 8 EN 20898-2, galvanised	
IST-	R (stainless steel)		
1	Expansion sleeve	Stainless steel A4	
		Stainless steel A4, cone coated	
2	Bolt		$\begin{array}{l} 20 N/mm^2, \ f_{yk} = 575 N/mm^2\\ 00 N/mm^2, \ f_{yk} = 560 N/mm^2\\ 50 N/mm^2, \ f_{yk} = 500 N/mm^2\\ 50 N/mm^2, \ f_{yk} = 450 N/mm^2 \end{array}$
3	Washer	Stainless steel A4	
4	Hexagon nut	Stainless steel A4, coated	
IST-	HCR (high corrosic	n resistant steel)	
1	Expansion sleeve	Stainless steel A4	
2	Bolt	High corrosion resistant steel, cone coa	ated
2	DUIL	M8, M10, M12, M16: f _{uk} = 80	$00N/mm^2$, f _{yk} = 640N/mm ²
3	Washer	High corrosion resistant steel	
4	Hexagon nut	High corrosion resistant steel, coated	

Annex 2

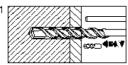
Materials

HST (steel galvanised) HST-R (stainless steel) HST-HCR (high corrosion resista	int steel)		M8	M10	M12	M16	M20 ¹⁾	M24 ¹⁾
Nominal diameter of drill bit	d ₀	[mm]	8	10	12	16	20	24
Cutting diameter of drill bit	$d_{cut} \leq$	[mm]	8,45	10,45	12,50	16,50	20,55	24,55
Depth of drill hole	h₁ ≥	[mm]	65	80	95	115	140	170
Diameter of clearance hole in the fixture	$d_f \leq$	[mm]	9	12	14	18	22	26
Effective anchorage depth	h _{ef}	[mm]	47	60	70	82	101	125
Torque moment	T _{inst}	[Nm]	20	45	60	110	240	300
Maximum thickness of fixture	t _{fix,max}	[mm]	195	200	200	235	305	330
Maximum length of anchor	I _{max}	[mm]	260	280	295	350	450	500
Shaft diameter at the cone	d _R	[mm]	5,5	7,2	8,5	11,6	14,6	17,4
Length of expansion sleeve	ls	[mm]	14,8	18,2	22,7	24,3	28,3	36,0
Width across flats	Sw	[mm]	13	17	19	24	30	36

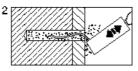
 $^{1)}$ Anchor size only for anchor types HST and HST-R $\,$



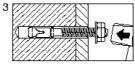
Setting instruction

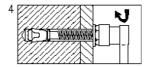


Drill hole with drill bit



Blow out dust and fragments





Install anchor

Apply tightening torque

Hilti stud anchor HST, HST-R, HST-HCR

Installation data, dimensions and setting instruction

Annex 3

Table 3: Minimum thickness of concrete member, minimum spacing and minimum edge distances

minimum edge dis									
HST (steel galvanised)			M8	M10	M12	M16	M20	M24	
Minimum thickness of concrete member	h _{min}	[mm]	100	120	140	160	200	250	
Cracked concrete									
Minimum spacing	S _{min}	[mm]	40	55	60	70	100	125	
Winning spacing	für c ≥	[mm]	50	70	75	100	160	180	
Minimum edge distance	C _{min}	[mm]	45	55	55	70	100	125	
	für s ≥	[mm]	50	90	120	150	225	240	
Non-cracked concrete									
Minimum spacing	S _{min}	[mm]	60	55	60	70	100	125	
	für c ≥	[mm]	50	80	85	110	225	255	
Minimum edge distance	C _{min}	[mm]	50	55	55	85	140	170	
	für s ≥	[mm]	60	115	145	150	270	295	
HST-R (stainless steel)			M8	M10	M12	M16	M20	M24	
Minimum thickness of concrete member	h _{min}	[mm]	100	120	140	160	200	250	
Cracked concrete									
Minimum spacing	S _{min}	[mm]	40	55	60	70	100	125	
Winimum spacing	für c ≥	[mm]	50	65	75	100	130	130	
Minimum edge distance	C _{min}	[mm]	45	50	55	60	100	125	
	für s ≥	[mm]	50	90	110	160	160	140	
Non-cracked concrete									
Minimum spacing	S _{min}	[mm]	60	55	60	70	100	125	
Minimum spacing	für c ≥	[mm]	60	70	80	110	195	205	
Minimum edge distance	C _{min}	[mm]	60	50	55	70	140	150	
	für s ≥	[mm]	60	115	145	160	210	235	
HST-HCR (high corrosion resist	ant steel)		M8	M10		M12	2	M16	
Minimum thickness of concrete member	h _{min}	[mm]	100		120	140		160	
Cracked concrete									
Minimum spacing	S _{min}	[mm]	40		55	60		70	
Minimum spacing	für c ≥	[mm]	50		70	75		100	
Minimum edge distance	C _{min}	[mm]	45		50	55		60	
winimum euge uisidhille	für s ≥	[mm]	50		90	110		160	
Non-cracked concrete									
Minimum spacing	S _{min}	[mm]	60		55	60		70	
	für c ≥	[mm]	50		70	80		110	
Minimum edge distance	C _{min}	[mm]	60		55	55		70	
winimum euge distance	für s ≥	[mm]	60	T	115	145	T	160	

Hilti stud anchor HST, HST-R, HST-HCR

Annex 4

Minimum thickness of concrete, minimum spacing and edge distances

HST (steel galvanised)			M8	M10	M12	M16	M20	M24
Steel failure								
Characteristic resistance	$N_{Rk,s}$	[kN]	19	32	43	75	75	127
Partial safety factor	γ _{Ms} ¹⁾	[-]			1,5			1,41
Pullout failure								
Characteristic resistance in cracked concrete C20/25	N _{Rk,p}	[kN]	5	9	12	20	30	40
Characteristic resistance in non-cracked concrete C20/25	$N_{Rk,p}$	[kN]	9	16	20	35	50	60
	ψ_{c}	C30/37			1,	22		
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete	ψ_{c}	C40/50			1,	41		
	ψ_{c}	C50/60			1,	55		
Partial safety factor	γ _{Mp} ¹⁾	[-]	1,8 ²⁾			1,5 ³⁾		
Concrete cone failure and splitting	failure							
Effective anchorage depth	h _{ef}	[mm]	47	60	70	82	101	125
Spacing	S _{cr,N} = S	_{cr,sp} [mm]			3>	k h _{ef}		
Edge distance	$C_{cr,N} = C$	_{cr,sp} [mm]			1,5	x h _{ef}		
Partial safety factor	$\gamma_{Mc} = \gamma_{Mc}$	¹⁾ [-]	1,8 ²⁾			1,5 ³⁾		
HST-R (stainless steel)			M8	M10	M12	M16	M20	M24
Steel failure								
Characteristic resistance	$N_{Rk,s}$	[kN]	17	28	40	69	109	156
Partial safety factor	γ _{Ms} ¹⁾	[-]		1,5		1,56	1,	73
Pullout failure								
Characteristic resistance in cracked concrete C20/25	N _{Rk,p}	[kN]	5	9	12	25	30	40
Characteristic resistance in	$N_{Rk,p}$	[kN]	9	16	20	35	50	60
non-cracked concrete C20/25		C30/37			1,	22		
	ψ_{c}	000/01						
Increasing factors for $N_{Rk,p}$ for	ψ _c Ψ _c	C40/50			1,	41		
	ψ _c ψ _c					41 55		
Increasing factors for $N_{Rk,p}$ for	ψ _c ψ _c	C40/50			1,			
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete	Ψc Ψc γ _{Mp} ¹⁾	C40/50 C50/60			1,	55		
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete Partial safety factor	Ψc Ψc γ _{Mp} ¹⁾	C40/50 C50/60	47	60	1,	55	101	125
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete Partial safety factor Concrete cone failure and splitting	$\frac{\psi_{c}}{\psi_{c}}$ $\frac{\gamma_{Mp}}{\gamma_{Mp}}^{1)}$ I failure	C40/50 C50/60 [-] [mm]	47	60	1, 1, 70	55 5 ³⁾	101	125
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete Partial safety factor Concrete cone failure and splitting Effective anchorage depth	$\frac{\psi_{c}}{\psi_{c}}$ $\frac{\gamma_{Mp}^{1)}}{\eta_{Mp}^{1}}$ $\frac{failure}{h_{ef}}$ $s_{cr,N} = s$	C40/50 C50/60 [-] [mm]	47	60	1, 1, 70 3 >	55 5 ³⁾ 82	101	125

Hilti stud anchor HST, HST-R, HST-HCR

Design method A, Characteristic values for tension loads

Annex 5

Table 5: Design method A Characteristic value	es for te	nsion loa	ads (cont	tinued)		
HST-HCR (high corrosion resista	nt steel)		M8	M10	M12	M16
Steel failure						
Characteristic resistance	N _{Rk,s}	[kN]	19,4	32,3	45,7	84,5
Partial safety factor	γ _{Ms} ¹⁾	[-]		1,	,5	
Pullout failure						
Characteristic resistance in cracked concrete C20/25	$N_{Rk,p}$	[kN]	5	9	12	25
Characteristic resistance in non-cracked concrete C20/25	$N_{Rk,p}$	[kN]	9	16	20	35
	ψ_{c}	C30/37		1,:	22	
Increasing factors for N _{Rk,p} for cracked and non-cracked concrete	ψ_{c}	C40/50		1,4	41	
	ψc	C50/60		1,	55	
Partial safety factor	γ _{Mp} ¹⁾	[-]		1,5	5 ²⁾	
Concrete cone failure and splittir	ng failure					
Effective anchorage depth	h _{ef}	[mm]	47	60	70	82
Spacing	$S_{cr,N} = S_{cr,s}$	_{sp} [mm]		3 x	h _{ef}	
Edge distance	$C_{cr,N} = C_{cr,s}$	_{sp} [mm]		1,5	x h _{ef}	
Partial safety factor	$\gamma_{Mc} = \gamma_{M,sp}$	¹⁾ [-]		1,5	5 ²⁾	

¹⁾ In absence of other national regulations.

²⁾ The partial safety factor $\gamma_2 = 1,0$ is included.

Hilti stud anchor HST, HST-R, HST-HCR

Annex 6

Design method A, Characteristic values for tension loads

Table 6: Displacements underHST (steel galvanised)			, M8	M10	M12	M16	M20	M24
Tension load in cracked concrete	N	[kN]	2	4,3	5,7	9,5	14,3	19,0
	δ_{N0}	[mm]	1,3	0,2	0,1	0,5	1,9	2,2
Corresponding displacement	δ _{N∞}	[mm]	1,2	1,0	1,2	1,2	2,3	2,5
Tension load in non-cracked concrete	Ν	[kN]	3,6	7,6	9,5	16,7	23,8	28,6
Corresponding displacement	δ_{N0}	[mm]	0,2	0,1	0,1	0,4	0,6	0,5
Corresponding displacement	δ_{N^∞}	[mm]	1,1	1,1	1,1	1,1	1,4	1,4
HST-R (stainless steel)			M8	M10	M12	M16	M20	M24
Tension load in cracked concrete	Ν	[kN]	2,4	4,36	5,7	11,9	14,30	19,0
Corresponding displacement	δ_{N0}	[mm]	0,6	0,2	0,8	1,0	1,1	0,8
Corresponding displacement	δ _{N∞}	[mm]	1,5	1,2	1,4	1,2	1,2	1,7
Tension load in non-cracked concrete	Ν	[kN]	4,3	7,6	9,5	16,7	23,8	28,6
Corresponding displacement	δ_{N0}	[mm]	0,1	0,1	0,1	0,1	0,5	0,8
corresponding displacement	δ_{N^∞}	[mm]	1,5	1,2	1,4	1,2	1,2	1,7
HST-HCR (high corrosion resistant s	teel)		M8		M10	M12		M16
Tension load in cracked concrete	Ν	[kN]	2,4		4,3	5,7		11,9
Corresponding displacement	δ_{N0}	[mm]	0,6		0,2	0,8		1,0
Corresponding displacement	δ_{N^∞}	[mm]	1,5		1,2	1,4		1,2
Tension load in non-cracked concrete	Ν	[kN]	4,3		7,6	9,5		16,7
Corresponding displacement	δ_{N0}	[mm]	0,1		0,1	0,1		0,1
Corresponding displacement	δ_{N^∞}	[mm]	1,5		1,2	1,4		1,2

Hilti stud anchor HST, HST-R, HST-HCR

Annex 7

Displacements under tension loads

HST (steel galvanised)			M8	M10	M12	M16	M20	M24
Steel failure without lever arm								
Characteristic resistance	$V_{Rk,s}$	[kN]	14	23,5	35	55	84	94
Partial safety factor	γ _{Ms} 1)	[-]			1,25			1,5
Steel failure with lever arm								
Characteristic resistance	$M^0_{\ Rk,s}$	[Nm]	30	60	105	240	454	595
Partial safety factor	γ _{Ms} 1)	[-]			1,25			1,5
Concrete pryout failure								
Factor in equation (5.6) of ETAG 001 Annex C, 5.2.3.3	k	[-]	2	,0	2,2	2,5	2,5	2,5
Partial safety factor	γ _{Mcp} ¹⁾	[-]			1,5	5 ²⁾		
Concrete edge failure								
Effective length of anchor in shear loading	_f	[mm]	47	60	70	82	101	125
Diameter of anchor	d _{nom}	[mm]	8	10	12	16	20	24
Partial safety factor	γ _{Mc} ¹⁾	[-]			1,5	5 ²⁾		
HST-R (stainless steel)			M8	M10	M12	M16	M20	M24
Steel failure without lever arm								
Characteristic resistance	$V_{Rk,s}$	[kN]	13	20	30	50	60	80
Partial safety factor	γ _{Ms} ¹⁾	[-]		1,25		1,3	1,4	44
Steel failure with lever arm								
Characteristic resistance	$M^0_{\ Rk,s}$	[Nm]	27	53	92	216	422	730
Partial safety factor	γ _{Ms} 1)	[-]		1,25		1,3	1,4	44
Concrete pryout failure								
Factor in equation (5.6) of ETAG 001 Annex C, 5.2.3.3	k	[-]			2	,0		
Partial safety factor	γ _{Mcp} ¹⁾	[-]			1,5	5 ²⁾		
Concrete edge failure								
Effective length of anchor in shear	l _f	[mm]	47	60	70	82	101	125
loading								
loading Diameter of anchor	d _{nom}	[mm]	8	10	12	16	20	24

¹⁾ In absence of other national regulations. ²⁾ The partial safety factor $\gamma_2 = 1,0$ is included.

Hilti stud anchor HST, HST-R, HST-HCR

Annex 8

Design method A, Characteristic values for shear loads

Table 8: Design method ACharacteristic values	for shea	ar loac	ls (contir	nued)		
HST-HCR (high corrosion resistant s	teel)		M8	M10	M12	M16
Steel failure without lever arm						
Characteristic resistance	$V_{Rk,s}$	[kN]	13	20	30	55
Partial safety factor	γ_{Ms} 1)	[-]		1,	25	
Steel failure with lever arm						
Characteristic resistance	$M^0_{Rk,s}$	[Nm]	30	60	105	266
Partial safety factor	γ _{Ms} 1)	[-]		1,:	25	
Concrete pryout failure						
Factor in equation (5.6) of ETAG 001 Annex C, 5.2.3.3	k	[-]		2	,0	
Partial safety factor	γ _{Mcp} ¹⁾	[-]		1,5	5 ²⁾	
Concrete edge failure						
Effective length of anchor in shear loading	l _f	[mm]	47	60	70	82
Diameter of anchor	d _{nom}	[mm]	8	10	12	16
Partial safety factor	γ _{Mc} ¹⁾	[-]		1,5	5 ²⁾	

¹⁾ In absence of other national regulations. ²⁾ The partial safety factor $\gamma_2 = 1,0$ is included.

Table 9: Displacement under shear loads

HST (steel galvanised)			M8	M10	M12	M16	M20	M24
Shear load in cracked and non-cracked concrete	V	[kN]	8,0	13,4	20,0	31,4	48,0	45,0
Corresponding displacement	δ_{V0}	[mm]	2,5	2,5	3,7	4,0	2,7	2,0
Corresponding displacement	δ_{V^∞}	[mm]	3,8	3,7	5,5	6,0	4,1	3,0
HST-R (stainless steel)			M8	M10	M12	M16	M20	M24
Shear load in cracked and non-cracked concrete	V	[kN]	7,4	11,0	17,0	27,5	40,0	57,0
	δ_{V0}	[mm]	1,6	3,3	4,9	2,2	2,5	2,5
Corresponding displacement	δ_{V^∞}	[mm]	2,4	4,9	7,4	3,3	3,7	3,7
HST-HCR (high corrosion resistant st	teel)		M8		M10	M12		M16
Shear load in cracked and non-cracked concrete	V	[kN]	7,4		11,0	17,0		27,5
	δ_{V0}	[mm]	1,6		3,3	4,9		2,2
Corresponding displacement	δ_{V^∞}	[mm]	2,4		4,9	7,4		3,3

Hilti stud anchor HST, HST-R, HST-HCR

Design method A, Characteristic values for shear loads **Displacement under shear loads**

Annex 9

Table 10:Design method A
Characteristic tension resistance in cracked and non-cracked
concrete C20/25 to C50/60 under fire exposure

HST (steel galvanised)				M8	M10	M12	M16	M20	M24
Steel failure					•				
	R30	$N_{Rk,s,fi}$	[kN]	0,9	2,5	5	9	15	20
Charactariatia registance	R60	N _{Rk,s,fi}	[kN]	0,7	1,5	3,5	6	10	15
Characteristic resistance	R90	N _{Rk,s,fi}	[kN]	0,6	1	2	3,5	6	8
	R120	N _{Rk,s,fi}	[kN]	0,5	0,7	1	2	3,5	5
Pullout failure									
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N _{Rk,p,fi}	[kN]	1,3	2,3	3	5	7,5	10
	R120	N _{Rk,p,fi}	[kN]	1,0	1,8	2,4	4	6	8
Concrete cone failure and	splitting	failure		-	-		-		-
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N ⁰ _{Rk,c,fi}	[kN]	2,7	5	7,3	10,9	18,3	31,3
	R120	N ⁰ _{Rk,c,fi}	[kN]	2,2	4	5,9	8,7	14,7	25
Spacing		S _{cr,N}	[mm]			1	h _{ef}	1	
opaoling		S _{min}	[mm]	40	55	60	70	100	125
		C _{cr,N}	[mm]				h _{ef}		
Edge distance		C _{min}	[mm]		ack from			-	
		Omin	[]	Fire att	ack from	n more t	han one	side: ≥ :	300
HST-R (stainless steel)				M8	M10	M12	M16	M20	M24
Steel failure					•		•		
	R30	N _{Rk,s,fi}	[kN]	4,9	11,8	17,2	32	49,9	71,9
Characteristic resistance	R60	N _{Rk,s,fi}	[kN]	3,6	8,4	12,2	22,8	35,5	51,2
Characteristic resistance	R90	N _{Rk,s,fi}	[kN]	2,4	5	7,3	13,5	21,1	30,4
	R120	N _{Rk,s,fi}	[kN]	1,7	3,3	4,8	8,9	13,9	20
Pullout failure									
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N _{Rk,p,fi}	[kN]	1,3	2,3	3	6,3	7,5	10
	R120	$N_{Rk,p,fi}$	[kN]	1	1,8	2,4	5	6	8
Concrete cone failure and	splitting	failure							
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N ⁰ _{Rk,c,fi}	[kN]	2,7	5	7,4	11	18,5	31,4
	R120	N ⁰ _{Rk,c,fi}	[kN]	2,2	4	5,9	8,8	14,8	25,2
Spacing		S _{cr,N}	[mm]			4 x	h _{ef}		
opaonig		S _{min}	[mm]	40	55	60	70	100	125
		C _{cr,N}	[mm]			2 x	h _{ef}		
Edge distance		C _{min}	[mm]		ack from ack from			-	300
n absence of other national regulation	ons the part	ial safety fac	tor for res	sistance u	nder fire ex	kposure γ	_{M,fi} = 1,0 is	recomme	ended.
ilti stud anchor HST, H			2			۸nr	nex 10		

Characteristic values of tension load resistance under fire exposure

Table 11: Design method A
Characteristic tension resistance in cracked and non-cracked
concrete C20/25 to C50/60 under fire exposure (continued)

HST-HCR (high corrosion r	esistant	steel)		M8	M10	M12	M16
Steel failure							
	R30	N _{Rk,s,fi}	[kN]	4,9	11,8	17,2	32
Characteristic resistance	R60	N _{Rk,s,fi}	[kN]	3,6	8,4	12,2	22,8
Characteristic resistance	R90	N _{Rk,s,fi}	[kN]	2,4	5	7,3	13,5
	R120	N _{Rk,s,fi}	[kN]	1,7	3,3	4,8	8,9
Pullout failure							
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N _{Rk,p,fi}	[kN]	1,3	2,3	3	6,3
	R120	N _{Rk,p,fi}	[kN]	1	1,8	2,4	5
Concrete cone failure and	splitting	failure					
Characteristic resistance in concrete ≥ C20/25	R30 R60 R90	N ⁰ _{Rk,c,fi}	[kN]	2,7	5	7,4	11
	R120	N ⁰ _{Rk,c,fi}	[kN]	2,2	4	5,9	8,8
Spacing		S _{cr,N}	[mm]		4 x	h _{ef}	
Spacing		S _{min}	[mm]	40	55	60	70
		C _{cr,N}	[mm]		2 x	: h _{ef}	
Edge distance		C _{min}	[mm]	2 x h _{ef}	from one sid		
				Fire attack	from more t	han one side	e: ≥ 300

In absence of other national regulations the partial safety factor for resistance under fire exposure $\gamma_{M,fi} = 1,0$ is recommended.

Hilti stud anchor HST, HST-R, HST-HCR

Annex 11

Characteristic values of tension load resistance under fire exposure

Table 12: Design method A
Characteristic shear resistance in cracked and non-cracked concrete
C20/25 to C50/60 under fire exposure

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c} \begin{array}{c} \begin{array}{c ccccccccccccccccccccccccccccccccccc$	HST (steel galvanised)				M8	M10	M12	M16	M20	M24
$\frac{1}{R60} = \frac{1}{V_{Rk,c,fi}} = \frac{1}{RN} = \frac{1}{O} = \frac$	$\frac{1}{R60} = \frac{1}{V_{Rk,s,fi}} = \frac{1}{[kN]} = \frac{1}{0} =$	Steel failure without lever	arm								
$ \frac{P60 V_{Rk,s,fi} [kN] 0,7 1,5 3,5 6 10 15 \\ \hline P90 V_{Rk,s,fi} [kN] 0,6 1 2 3,5 6 8 \\ \hline P120 V_{Rk,s,fi} [kN] 0,6 1 2 3,5 6 8 \\ \hline P120 V_{Rk,s,fi} [kN] 0,5 0,7 1 2 3,5 5 \\ \hline Steel failure with lever arm \\ \hline P120 V_{Rk,s,fi} [kN] 1 3,3 8,1 20,6 40,2 69,7 \\ \hline P120 M^0_{Rk,s,fi} [Nm] 1 3,3 8,1 20,6 40,2 69,7 \\ \hline P120 M^0_{Rk,s,fi} [Nm] 0,8 2,4 5,7 14,4 28,1 48,7 \\ \hline P90 M^0_{Rk,s,fi} [Nm] 0,7 1,6 3,2 8,2 16 27,7 \\ \hline P120 M^0_{Rk,s,fi} [Nm] 0,6 1,2 2 5,1 9,9 17,7 \\ \hline Concrete pryout failure \\ \hline Factor in equation (5.6) of ETAG 001 k [-1] 2,0 2,0 2,2 2,5 2,5 2,5 \\ \hline Characteristic resistance \hline P300 V_{Rk,cp,fi} [kN] 5,4 10 16 27,2 49,4 84,7 \\ \hline P120 V_{Rk,cp,fi} [kN] 4,4 8 12,9 21,7 39,6 67,7 \\ \hline Concrete edge failure \\ \hline The initial value V^0_{Rk,c,fi} of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: \\ V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c} (\leq P90) V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c} (R120) \\ \hline with V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c} (\leq P90) V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c} (R120) \\ \hline with V^0_{Rk,c,fi} = 1,0 is \\ \hline D 000000000000000000000000000000000$	$ \frac{R60 V_{Rk,s,fi} [kN] 0,7 1,5 3,5 6 10 15}{R90 V_{Rk,s,fi} [kN] 0,6 1 2 3,5 6 8}{R120 V_{Rk,s,fi} [kN] 0,6 1 2 3,5 6 8} \\ \hline R120 V_{Rk,s,fi} [kN] 0,5 0,7 1 2 3,5 5 \\ \hline \textbf{Steel failure with lever arm} \\ \hline \textbf{Characteristic resistance} \frac{R30 M^0_{Rk,s,fi} [Nm] 1 3,3 8,1 20,6 40,2 69,5}{R60 M^0_{Rk,s,fi} [Nm] 0,8 2,4 5,7 14,4 28,1 48,6 \\ \hline \textbf{R90 M^0_{Rk,s,fi} [Nm] 0,8 2,4 5,7 14,4 28,1 48,6 \\ \hline \textbf{R90 M^0_{Rk,s,fi} [Nm] 0,7 1,6 3,2 8,2 16 27,7 \\ \hline \textbf{R120 M^0_{Rk,s,fi} [Nm] 0,6 1,2 2 5,1 9,9 17,7 \\ \hline \textbf{Concrete pryout failure} \\ \hline \textbf{Factor in equation (5.6) of ETAG 001 k [-] 2,0 2,0 2,2 2,5 2,5 2,5 \\ \hline \textbf{Characteristic resistance} \hline \begin{array}{c} \textbf{R30 \\ \textbf{R60 \\ \textbf{R90 } \textbf{V}_{Rk,cp,fi} [kN] 5,4 10 16 27,2 49,4 84,7 \\ \hline \textbf{R120 V_{Rk,cp,fi} [kN] 5,4 10 16 27,2 49,4 84,7 \\ \hline \textbf{R120 V_{Rk,cp,fi} [kN] 4,4 8 12,9 21,7 39,6 67,7 \\ \hline \textbf{Concrete edge failure} \\ \hline \textbf{The initial value $V^0_{Rk,c,fi}$ of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: \\ V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c} (\leq R90) V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c} (R120) \\ \hline \textbf{with $V^0_{Rk,c,fi}$ of the characteristic resistance in cracked concrete C20/25 under normal temperature. \\ \hline \textbf{mabsence of other national regulations the partial safety factor for resistance under fire exposure $\gamma_{M,fi} = 1,0$ is } \ \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 1,0$ is \\ \hline \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 0,0 \textbf{Material} = 0,0 Ma$		R30	V _{Rk,s,fi}	[kN]	0,9	2,5	5	9	15	20
$ \frac{\text{R90}}{\text{R120}} \frac{\text{V}_{\text{Rk},\text{s},\text{fi}}}{\text{R120}} \frac{\text{[kN]}}{\text{V}_{\text{Rk},\text{s},\text{fi}}} \frac{\text{[kN]}}{\text{[kN]}} 0,5 0,7 1 2 3,5 6 8 \\ \hline \hline \text{R120} V_{\text{Rk},\text{s},\text{fi}} \frac{\text{[kN]}}{\text{[kN]}} 0,5 0,7 1 2 3,5 5 \\ \hline \text{Steel failure with lever arm} \\ \hline \begin{array}{c} \frac{\text{R30}}{\text{R60}} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{1} 1 3,3 8,1 20,6 40,2 69,1 \\ \hline \hline \text{R60} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{1} 0,8 2,4 5,7 14,4 28,1 48,1 \\ \hline \hline \text{R90} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{10} 0,7 1,6 3,2 8,2 16 27,7 \\ \hline \hline \text{R120} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{10} 0,6 1,2 2 5,1 9,9 17,1 \\ \hline \text{Concrete pryout failure} \\ \hline \text{Factor in equation (5.6) of ETAG 001} k \left[\cdot\right] 2,0 2,0 2,2 2,5 2,5 2,5 \\ \hline \text{Characteristic resistance} \hline \begin{array}{c} \frac{\text{R30}}{\text{R60}} V_{\text{Rk},\text{cp},\text{fi}} \frac{\text{[kN]}}{10} 5,4 10 16 27,2 49,4 84,1 \\ \hline \text{R120} V_{\text{Rk},\text{cp},\text{fi}} \frac{\text{[kN]}}{10} 4,4 8 12,9 21,7 39,6 67,1 \\ \hline \text{Concrete edge failure} \\ \hline \text{The initial value V}^0_{\text{Rk},\text{c,fi}} of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: \\ V^0_{\text{Rk},\text{c,fi}} = 0,25 \times V^0_{\text{Rk},\text{c}} (\leq \text{R90}) V^0_{\text{Rk},\text{c,fi}} = 0,20 \times V^0_{\text{Rk},\text{c}} (\text{R120}) \\ \text{with V}^0_{\text{Rk},\text{c,fi}} = 0,25 \times V^0_{\text{Rk},\text{c}} (\leq \text{R90}) V^0_{\text{Rk},\text{c,fi}} = 0,20 \times V^0_{\text{Rk},\text{c}} (\text{R120}) \\ \text{with V}^0_{\text{Rk},\text{c}} \text{ initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.} \\ \text{absence of other national regulations the partial safety factor for resistance under fire exposure } \gamma_{\text{M,fi}} = 1,0 \text{ is } \end{array} \right$	$ \frac{\text{R90}}{\text{R120}} \frac{\text{V}_{\text{Rk},\text{s},\text{fi}}}{\text{R120}} \frac{\text{[kN]}}{\text{0},\text{6}} \frac{1}{1} \frac{2}{2} \frac{3,5}{5} \frac{6}{6} \frac{8}{8} \\ \hline \text{R120} \text{V}_{\text{Rk},\text{s},\text{fi}} \frac{\text{[kN]}}{\text{[kN]}} \frac{0,6}{0,5} \frac{1}{0,7} \frac{1}{1} \frac{2}{2} \frac{3,5}{5} \frac{5}{5} \\ \hline \text{Steel failure with lever arm} \\ \hline \begin{array}{c} \frac{\text{R30}}{\text{R60}} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{1} \frac{1}{3,3} \frac{3,1}{8,1} \frac{20,6}{40,2} \frac{40,2}{69,5} \\ \hline \frac{860}{\text{R60}} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{1} \frac{1}{0,8} \frac{3,2}{2,4} \frac{4,2}{5,7} \frac{14,4}{28,1} \frac{48,6}{28,1} \\ \hline \frac{\text{R90}}{\text{R120}} M^0_{\text{Rk},\text{s},\text{fi}} \frac{\text{[Nm]}}{10} 0,7 1,6 3,2 8,2 16 27,7 \\ \hline \begin{array}{c} \text{Concrete pryout failure} \\ \hline \text{Factor in equation (5.6) of ETAG 001} \\ \hline \text{Annex C}, 5.2.3.3 \\ \hline \text{Characteristic resistance} \\ \hline \begin{array}{c} \frac{\text{R30}}{\text{R00}} V_{\text{Rk},\text{cp,fi}} \frac{\text{[kN]}}{10} 5,4 10 16 27,2 49,4 84,5 \\ \hline \text{R120} V_{\text{Rk},\text{cp,fi}} \frac{\text{[kN]}}{10} 4,4 8 12,9 21,7 39,6 67,5 \\ \hline \begin{array}{c} \text{Concrete edge failure} \\ \hline \text{The initial value V}^0_{\text{Rk},\text{c,fi}} \text{of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: \\ V^0_{\text{Rk},\text{c,fi}} = 0,25 \times V^0_{\text{Rk},\text{c}} (\leq \text{R90}) V^0_{\text{Rk},\text{c,fi}} = 0,20 \times V^0_{\text{Rk},\text{c}} (\text{R120}) \\ \hline \text{with V}^0_{\text{Rk},\text{c},\text{initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.} \\ \hline \text{absence of other national regulations the partial safety factor for resistance under fire exposure } \gamma_{\text{M,fi}} = 1,0 \text{ is } \end{array} $		R60		[kN]	0,7	1,5	3,5	6	10	15
$\frac{R_{RKS,fi}}{R_{RKS,fi}} [Nm] (NM] (NM) (NM) (NM) (NM) (NM) (NM) (NM) (NM)$	$\frac{R_{R,S,fi}}{R_{R,S,fi}} [NM] = 0, 0 = 0, 1 = 1 = 2 = 0, 0 = 0$ Steel failure with lever arm $\frac{R_{R,S,fi}}{R_{R,S,fi}} [NM] = 1 = 3, 3 = 8, 1 = 20, 6 = 40, 2 = 69, 40, 40, 40, 40, 40, 40, 40, 40, 40, 40$	Characteristic resistance	R90	V _{Rk,s,fi}	[kN]	0,6	1	2	3,5	6	8
$\begin{array}{c} \begin{array}{c} \begin{array}{c} R30 & M^{0}_{Rk,s,fi} & [Nm] & 1 & 3,3 & 8,1 & 20,6 & 40,2 & 69,1 \\ \hline R60 & M^{0}_{Rk,s,fi} & [Nm] & 0,8 & 2,4 & 5,7 & 14,4 & 28,1 & 48,1 \\ \hline R90 & M^{0}_{Rk,s,fi} & [Nm] & 0,7 & 1,6 & 3,2 & 8,2 & 16 & 27,7 \\ \hline R120 & M^{0}_{Rk,s,fi} & [Nm] & 0,6 & 1,2 & 2 & 5,1 & 9,9 & 17,2 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} concrete pryout failure \\ \hline \\ Factor in equation (5.6) of ETAG 001 \\ Annex C, 5.2.3.3 \\ \hline \\ Characteristic resistance \\ \hline \\ R120 & V_{Rk,cp,fi} & [kN] & 5,4 & 10 & 16 & 27,2 & 49,4 & 84,2 \\ \hline \\ R120 & V_{Rk,cp,fi} & [kN] & 5,4 & 10 & 16 & 27,2 & 49,4 & 84,2 \\ \hline \\ \hline \\ R120 & V_{Rk,cp,fi} & [kN] & 4,4 & 8 & 12,9 & 21,7 & 39,6 & 67,2 \\ \hline \\ $	$\begin{array}{c} \begin{array}{c} \begin{array}{c} R30 & M^{0}_{Rk,s,fi} & [Nm] & 1 & 3,3 & 8,1 & 20,6 & 40,2 & 69,8 \\ \hline R60 & M^{0}_{Rk,s,fi} & [Nm] & 0,8 & 2,4 & 5,7 & 14,4 & 28,1 & 48,6 \\ \hline R90 & M^{0}_{Rk,s,fi} & [Nm] & 0,7 & 1,6 & 3,2 & 8,2 & 16 & 27,7 \\ \hline R120 & M^{0}_{Rk,s,fi} & [Nm] & 0,6 & 1,2 & 2 & 5,1 & 9,9 & 17,2 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} concrete pryout failure \\ \hline \end{array} \\ \hline \begin{array}{c} Factor in equation (5.6) of ETAG 001 \\ Annex C, 5.2.3.3 & k & [-1] & 2,0 & 2,0 & 2,2 & 2,5 & 2,5 & 2,5 \\ \hline \end{array} \\ \hline \begin{array}{c} R30 \\ R60 \\ R90 \\ \hline \end{array} \\ \hline \begin{array}{c} R30 \\ R60 \\ R90 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} R30 \\ R60 \\ R90 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} R120 \\ V_{Rk,cp,fi} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} [kN] \\ 5,4 \\ 10 \\ 16 \\ 27,2 \\ 49,4 \\ 84,5 \\ \hline \end{array} \\ \hline \begin{array}{c} R120 \\ V_{Rk,cp,fi} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} R120 \\ V_{Rk,cp,fi} \\ \hline \end{array} \\ \hline \begin{array}{c} R120 \\ V_{Rk,cp,fi} \\ \hline \end{array} \\ \hline \begin{array}{c} R120 \\ V_{Rk,c,fi} \\ \hline \end{array} $ \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \bigg \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \end{array} \\ \hline \bigg \\ \hline \bigg \\ \hline \end{array} \\ \hline \end{array} \\ \\ \end{array} \\ \hline \end{array} \\ \\ \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \bigg \\ \hline \bigg \\ \hline \end{array} \\ \hline \bigg \\ \hline \end{array} \\ \hline \bigg \\ \hline \end{array} \\ \hline \bigg \\ \hline \bigg \\ \hline \bigg \\ \hline \end{array} \\ \hline \bigg \\ \hline \bigg \\ \hline \bigg \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \end{array} \\ \\ \end{array} \\ \hline \end{array} \\ \\ \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \\ \end{array} \\ \\ \end{array} \\ \\ \end{array} \\ \hline \end{array} \\ \\ \end{array} \\ \\ \\ \end{array} \\ \\ \\ \\ \end{array} \\ \\ \end{array} \\ \\ \end{array}		R120	V _{Rk,s,fi}	[kN]	0,5	0,7	1	2	3,5	5
$\begin{array}{c} \begin{array}{c} \hline R60 & M^{0}_{Rk,s,fi} & [Nm] & 0,8 & 2,4 & 5,7 & 14,4 & 28,1 & 48, \\ \hline R90 & M^{0}_{Rk,s,fi} & [Nm] & 0,7 & 1,6 & 3,2 & 8,2 & 16 & 27, \\ \hline R120 & M^{0}_{Rk,s,fi} & [Nm] & 0,6 & 1,2 & 2 & 5,1 & 9,9 & 17, \\ \hline \end{array} \\ \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \hline \end{array} $ \\ \hline \rule \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \end{aligned} \\ \\ \hline \bigg \\ \\ \\ \hline \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \\ \\ \hline \\ \\ \hline \end{array} \\ \hline \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \\ \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \hline \\ \\ \hline \end{array} \\ \hline \end{array} \\ \\ \hline \end{array} \\ \\ \hline \end{array} \\ \hline \\ \hline \\ \hline \end{array} \\ \hline \\ \\ \hline \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \hline \end{array} \\ \\ \hline \\ \\ \\ \\ \hline \\ \\ \hline \\ \\ \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \\ \\ \hline \\ \\ \\ \hline \\	$\begin{array}{c} \begin{array}{c} \hline R60 & M^{0}_{Rk,s,fi} & [Nm] & 0,8 & 2,4 & 5,7 & 14,4 & 28,1 & 48,0 \\ \hline R90 & M^{0}_{Rk,s,fi} & [Nm] & 0,7 & 1,6 & 3,2 & 8,2 & 16 & 27,7 \\ \hline R120 & M^{0}_{Rk,s,fi} & [Nm] & 0,6 & 1,2 & 2 & 5,1 & 9,9 & 17,2 \\ \hline \end{array}$	Steel failure with lever arn	n								
$\begin{tabular}{ c c c c c c c } \hline \begin{tabular}{ c c c c c c c } \hline \end{tabular} $	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$		R30	M ⁰ _{Rk,s,fi}	[Nm]	1	3,3	8,1	20,6	40,2	69,
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$		R60	${\sf M}^0_{{\sf Rk},{\sf s},{\sf fi}}$	[Nm]	0,8	2,4	5,7	14,4	28,1	48,
$\frac{\text{R}_{\text{R},\text{S},\text{fi}}}{\text{Concrete pryout failure}} = \frac{1}{2,0} = \frac{1}{2,0$	$\frac{\text{R}_{\text{R},\text{S},\text{fi}}}{\text{Concrete pryout failure}} = \frac{1}{2,0} = \frac{1}{2,0$	naracteristic resistance	R90		[Nm]	0,7	1,6	3,2	8,2	16	27,
Factor in equation (5.6) of ETAG 001 k [-] 2,0 2,0 2,2 2,5 2,5 2,5 2,5 2,5 2,5 2,5 2,5 2,5	Factor in equation (5.6) of ETAG 001 k [-] 2,0 2,0 2,2 2,5 2,5 2,5 2,5 2,5 2,5 2,5 2,5 2,5		R120	${\sf M}^0_{{\sf Rk},{\sf s},{\sf fi}}$	[Nm]	0,6	1,2	2	5,1	9,9	17,
Annex C, 5.2.3.3K[-]2,02,02,22,52,52,5Characteristic resistance $\begin{array}{cccccccccccccccccccccccccccccccccccc$	Annex C, 5.2.3.3K[-]2,02,02,22,52,52,5Characteristic resistance $\begin{array}{cccccccccccccccccccccccccccccccccccc$	Concrete pryout failure									
$\begin{array}{c} \begin{array}{c} \begin{array}{c} R60 \\ R90 \end{array} V_{Rk,cp,fi} & [kN] \end{array} 5,4 & 10 & 16 & 27,2 & 49,4 & 84,4 \\ \hline R120 & V_{Rk,cp,fi} & [kN] & 4,4 & 8 & 12,9 & 21,7 & 39,6 & 67,4 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} Concrete \ edge \ failure \end{array} \\ \hline \begin{array}{c} Phe \ initial \ value \ V^0_{Rk,c,fi} \ of \ the \ characteristic \ resistance \ in \ concrete \ C20/25 \ to \ C50/60 \ under \ fire \ exposure \ may \ be \ determined \ by: \\ V^0_{Rk,c,fi} \ = \ 0,25 \ x \ V^0_{Rk,c} (\leq R90) \\ \hline \end{array} \\ \hline V^0_{Rk,c,fi} \ = \ 0,20 \ x \ V^0_{Rk,c} (R120) \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} V^0_{Rk,c,fi} \ = \ 0,20 \ x \ V^0_{Rk,c} (R120) \\ \hline \end{array} \\ \hline \begin{array}{c} Phe \ resistance \ of \ other \ national \ regulations \ the \ partial \ safety \ factor \ for \ resistance \ under \ fire \ exposure \ under \ fire \ exposure \ resistance \ resistance \ under \ resistance \ restance \ restance \ resistance \ resistance \ restance \ $	$\begin{array}{c} \begin{array}{c} \begin{array}{c} R60 \\ R90 \end{array} V_{Rk,cp,fi} & [kN] \end{array} 5,4 & 10 & 16 & 27,2 & 49,4 & 84,4 \\ \hline R120 & V_{Rk,cp,fi} & [kN] & 4,4 & 8 & 12,9 & 21,7 & 39,6 & 67,4 \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} Concrete \ edge \ failure \end{array} \\ \hline \begin{array}{c} Phe \ initial \ value \ V^0_{Rk,c,fi} \ of \ the \ characteristic \ resistance \ in \ concrete \ C20/25 \ to \ C50/60 \ under \ fire \ exposure \ may \ be \ determined \ by: \\ V^0_{Rk,c,fi} \ = \ 0,25 \ x \ V^0_{Rk,c} (\leq R90) \\ \hline \end{array} \\ \hline V^0_{Rk,c,fi} \ = \ 0,20 \ x \ V^0_{Rk,c} (R120) \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} V^0_{Rk,c,fi} \ = \ 0,20 \ x \ V^0_{Rk,c} (R120) \\ \hline \end{array} \\ \hline \begin{array}{c} Phe \ resistance \ of \ other \ national \ regulations \ the \ partial \ safety \ factor \ for \ resistance \ under \ fire \ exposure \ under \ fire \ exposure \ resistance \ resistance \ under \ resistance \ restance \ restance \ resistance \ resistance \ restance \ $	• • • •	TAG 001	k	[-]	2,0	2,0	2,2	2,5	2,5	2,5
Concrete edge failure The initial value $V^0_{Rk,c,fi}$ of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: $V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c}$ ($\leq R90$) $V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c}$ (R120) with $V^0_{Rk,c}$ initial value of the characteristic resistance in cracked concrete C20/25 under normal remperature.	Concrete edge failure The initial value $V^0_{Rk,c,fi}$ of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: $V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c}$ ($\leq R90$) $V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c}$ (R120) with $V^0_{Rk,c}$ initial value of the characteristic resistance in cracked concrete C20/25 under normal remperature.	Characteristic resistance	R60	V _{Rk,cp,fi}	[kN]	5,4	10	16	27,2	49,4	84,
The initial value $V^0_{Rk,c,fi}$ of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: $V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c}$ ($\leq R90$) $V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c}$ (R120) with $V^0_{Rk,c}$ initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.	The initial value $V^0_{Rk,c,fi}$ of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by: $V^0_{Rk,c,fi} = 0,25 \times V^0_{Rk,c}$ ($\leq R90$) $V^0_{Rk,c,fi} = 0,20 \times V^0_{Rk,c}$ (R120) with $V^0_{Rk,c}$ initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.		R120	$V_{Rk,cp,fi}$	[kN]	4,4	8	12,9	21,7	39,6	67,
			ulations the	e partial saf	ety facto	r for resi	stance u	nder fire	exposure	$\gamma_{M,fi} = 1$	0 is
		ilti stud anchor HST,	HST-R, I	HST-HCI	R			Anr	nex 12		
ilti stud anchor HST, HST-R, HST-HCR Annex 12	ilti stud anchor HST, HST-R, HST-HCR Annex 12	Characteristic valu	ues of sh	near load	t racio	tanco			uropea		

ETA-98/0001

Table 13:Design method A
Characteristic shear resistance in cracked and non-cracked concrete
C20/25 to C50/60 under fire exposure (continued)

HST-R (stainless steel)				M8	M10	M12	M16	M20	M24
Steel failure without lever	arm							<u>.</u>	<u>.</u>
Characteristic resistance	R30	$V_{Rk,s,fi}$	[kN]	4,9	11,8	17,2	32	49,9	71,9
	R60	$V_{Rk,s,fi}$	[kN]	3,6	8,4	12,2	22,8	35,5	51,2
	R90	$V_{Rk,s,fi}$	[kN]	2,4	5	7,3	13,5	21,1	30,4
	R120	$V_{Rk,s,fi}$	[kN]	1,7	3,3	4,8	8,9	13,9	20
Steel failure with lever arn	n								
Characteristic resistance	R30	${\sf M}^0_{{\sf Rk},{\sf s},{\sf fi}}$	[Nm]	5	15,2	26,6	67,7	132,3	228,6
	R60	${\sf M}^0_{{\sf Rk},{\sf s},{\sf fi}}$	[Nm]	3,7	10,8	19	48,2	94,1	162,6
	R90	${\sf M}^0_{{\sf Rk},{\sf s},{\sf fi}}$	[Nm]	2,4	6,4	11,3	28,6	55,9	96,6
	R120	M ⁰ _{Rk,s,fi}	[Nm]	1,8	4,2	7,4	18,9	36,8	63,7
Concrete pryout failure									
$V^{0}_{Rk,c,fi} = 0,25 \times V^{0}_{Rk}$	_{k,c} (≤ R90))	V ⁰ _{Rk,c,fi} =	= 0,20 x	V ⁰ _{Rk,c}	(R120)			
$V^{0}_{Rk,c,fi} = 0,25 \times V^{0}_{Rk}$ with $V^{0}_{Rk,c}$ initial value of the temperature.	character	istic resista	ance in	cracked	l concret	e C20/2			.0 is

Hilti stud anchor HST, HST-R, HST-HCR

Annex 13

Characteristic values of shear load resistance under fire exposure

Table 14:Design method A
Characteristic shear resistance in cracked and non-cracked concrete
C20/25 to C50/60 under fire exposure (continued)

HST-HCR (high corrosion resistant steel)					M10	M12	M16		
Steel failure without lever arm									
Characteristic resistance	R30	V _{Rk,s,fi}	[kN]	4,9	11,8	17,2	32		
	R60	$V_{Rk,s,fi}$	[kN]	3,6	8,4	12,2	22,8		
	R90	V _{Rk,s,fi}	[kN]	2,4	5	7,3	13,5		
	R120	V _{Rk,s,fi}	[kN]	1,7	3,3	4,8	8,9		
Steel failure with lever arn	n								
Characteristic resistance	R30	M ⁰ _{Rk,s,fi}	[Nm]	5	15,2	26,6	67,7		
	R60	М ⁰ _{Rk,s,fi}	[Nm]	3,7	10,8	19	48,2		
	R90	M ⁰ _{Rk,s,fi}	[Nm]	2,4	6,4	11,3	28,6		
	R120	M ⁰ _{Rk,s,fi}	[Nm]	1,8	4,2	7,4	18,9		
Concrete pryout failure									
In equation (5.6) of ETAG 0 Table 9 have to be consider		C, 5.2.3.3	the k-fa	ctor 2,0 an	d the relevar	nt values N ⁰ _F	_{Rk,c,fi} Of		
Concrete edge failure									
The initial value $V^0_{Rk,c,fi}$ of th	e characte	eristic resis	tance in	concrete (C20/25 to C5	0/60 under f	ire		

exposure may be determined by: $V_{Rk,c,fi}^{0} = 0.25 \times V_{Rk,c}^{0}$ ($\leq R90$) $V_{Rk,c,fi}^{0} = 0.20 \times V_{Rk,c}^{0}$ (R120) with $V_{Rk,c,fi}^{0}$ is introduced as a statement of the scheme transition are shown in a statement of the scheme transition.

with $V^0_{Rk,c}$ initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.

In absence of other national regulations the partial safety factor for resistance under fire exposure $\gamma_{M,fi} = 1,0$ is recommended.

Hilti stud anchor HST, HST-R, HST-HCR

Annex 14

Characteristic values of shear load resistance under fire exposure